

E R R A T A

“Estimating Room Temperatures and the Likelihood of
Flashover Using Fire Test Data Correlations”

B. J. McCaffrey, J. G. Quintiere, and M. F. Harkleroad

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- p. 111 Figure 3, upper caption — next to $h_k = 0.0055 \text{ kW/m}^2\text{K}$, replace $t = 1000 \text{ sec}$ by $\delta = 0.031 \text{ m}$. Otherwise figure is correct.
- p. 113 Figure 4 — The calculation inadvertently used a characteristic time of 1 s as opposed to 1000 s. Although not very realistic physically the figure is correct for the 1 s time. To convert to a more sensible time of 1000 s the value of h_k contained in the brackets beside the names of the lining material should be divided by $\sqrt{1000}$ and the ordinate, Q , should be divided by $(1000)^{1/4}$. The qualitative picture implied by the figure remains the same. (The value of h_k given for Expanded Polystyrene should read 0.032 and the compartment size should read 2 m \times 6 m \times 2.4 m high).
- p. 114 Nomenclature — A_w , replace by $2(L \times H + L \times W + H \times W)$
- p. 116 Appendix 1, first line — replace “The variable will . . .” by “The variable *which* will . . .”
- p. 118 Equation B-1 should read:

$$T_x/T_s = \exp [-(X^*)^2] - \sqrt{\pi} X^* \operatorname{erfc} (X^*)$$

- p. 118 Second to last line — replace $\frac{1}{\alpha} \left(\frac{\sigma}{2}\right)^2$ by $\frac{1}{\alpha} \left(\frac{\delta}{2}\right)^2$